

Thermoelectricity: From Atoms to Systems

Week 4: Thermoelectric Systems Lecture 4.2: Thermoelectric cost/efficiency Trade off

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Solar Cells (Efficiency+ Cost \rightarrow \$/W) US\$0.50/W US\$0.10/W US\$0.20/W 100 3rd generation low-Thermodynamic cost high efficiency limit 80 Efficiency,% 60 US\$1.00/W 40 Present limit 20US\$3.50/W 100 400 500 200 300 1st generation high-cost Cost, US\$/m² 2nd generation low-cost medium efficiency low efficiency We need to estimate the cost of TE system

per surface area of the heat source (\$/m²)



Model of TE module + heat exchanger for cost/efficiency trade off analysis



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K. Yazawa and A. Shakouri, Env. Science and Technology (July 2011)
J. Appl. Phys. 111, 024509 (2012)

TE module and the heat sink need to be cooptimized to get the highest output power (thermal impedance matching).





Maximum power output

Thermal-electrical co-optimization

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K. Yazawa and A. Shakouri, Env. Science and Technology (July 2011)

Heat sink optimization

Micro-channel heat sinks

$$U_{BASE} A_{BASE} = 1 / \left(\frac{1}{2\rho C_p G} + \frac{1}{U_{fin} A_{fin}} \right)$$

Matched pumping power

$$w_{pp} = 3\mu \left(\frac{N_u k_f}{\rho C_p}\right)^2 \frac{(H+\delta)^6}{(b+\delta)(H\delta)^5} L^2$$

L:length of channel

Nusselt number

 $Nu = 4.52 * (1 - \delta / H)^{3.78} + 2.98$

Optimum design: matched resistance based on convection from fin surface and sensitive heat of fluid.

Yazawa and Shakouri, Env. Science and Technology (July 2011)

Components of TE system (cost per unit area)

Use of heat spreading inside TE module (thermal concentration)

F= Fractional area coverage = Area of TE legs divided by area of the heat source

T_{source}, Input heat flux

Yazawa and Shakouri, Env. Science and Technology (July 2011)

Fractional area factor

Heat concentration => Less TE material use

Spreading thermal resistance,

$$\psi_{sh} = \psi_{sc} = \frac{\lambda}{\beta_s a (1 + 2\lambda \tan \phi)}$$

where angle ϕ is,

 $\begin{cases} \phi = 5.86 \ln(\lambda) + 40.4 & 0.0011 < \lambda \le 1 \\ \phi = 46.45 - 6.048 \lambda^{-0.969} & \lambda \ge 1 \end{cases}$ $\lambda = d_s / a$

Vermeersch et al, J of HT, 2008

 $F = \left(1 - \frac{2d_s \tan \phi}{a}\right)^2$ F: fractional area factor (Fill factor) (Fill factor)

Yazawa and Shakouri, Env. Science and Technology (July 2011)

Cost per unit area for TE bottom cycle waste heat recovery (TE module + heat sink)

ZT=1, β =1.5 W/mK β_{sub} =100 W/mK t_{sub} =0.2mm

 T_{s} =600K, T_{a} =300K Fan efficiency 30%

TE (BiTe or PbTe): \$500/kg Substrate-AIN: \$100/kg AI: \$8/kg Cu: \$20/kg

K. Yazawa and A. Shakouri, Env. Science & Technology (July 2011)

Fractional area coverage in TE module plays a big role to reduce the overall cost.High input heat fluxes require much less TE material (thermal impedance matching)

TE Module/Heat Sink Material Cost per Watt (car exhaust application)

\$500/kg,

\$ 5/kg,

\$ 20/kg

 U_{h} =4.6x10²W/m²K

Yazawa & Shakouri; Journal of Material Research 2012

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• TE material with ZT=0.5-1 can have a big impact in high heat flux waste heat recovery applications if the source of heat is free (neglect impact on the topping cycle).

TE for topping cycle applications

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TE / Steam Turbine combined cycle (Quest)

• With today's steam temperatures (775-825K), material with ZT=0.3-1 can have a big impact to increase the overall power plant efficiency (+2.6% to +8.2%).

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TE/Steam Turbine Energy Cost

Yazawa & Shakouri, Applied Energy, 2013

Simplified Steam Turbine Model

Material with ZT=0.3-1 (even at a cost of \$500/kg) can have a big impact to improve the energy economy of the TE topping cycle power plants.

Detailed Coal-Fired Power Plant Model

• TE module optimized based on temperature and heat flux at each location on the wall of the boiler.

VISUALIZATION & SIMULATION

Topping Cycle TE Coal-Fired Power Plant

	Gas Temperature (K)			
	1680	1500	1300	1150
Leg thickness (mm)	0.3	0.4	0.5	0.55
Fin height (mm)	4.3	4.4	3.8	3.4
T _h (K)	1439.8	1284.4	1104.1	977.1
T _c (K)	1213.4	1067.6	927.2	842.8
ZT	0.88	0.78	0.73	0.61
$w_{TE,leg} (W/m^2)$	4.17x10 ⁴	2.88x10 ⁴	1.54x10 ⁴	8.08x10 ³
$w_{TE} (W/m^2)$	1.65x10 ⁴	1.14×10^{4}	6.10x10 ³	3.21x10 ³
η_{TE}	3.5%	3.4%	2.8%	2.1%
W_{steam} (W/m ²)	2.26x10 ⁵	1.62×10^{5}	1.07x10 ⁵	7.36x10 ⁴
w _o (W/m ²)	2.26x10 ⁵	1.62x10 ⁵	1.07x10 ⁵	7.36x10 ⁴
$w_{total} (W/m^2)$	2.42x10 ⁵	1.74x10 ⁵	1.13x10 ⁵	7.68x10 ⁴
Δw	7.1%	7.0%	5.6%	4.4%

TE leg thermal conductivity (β)	1.5	W/m-K
TE leg electric conductivity (σ)	25000	1/ Ω- m
TE density (ρ)	8200	kg/m ³
TE leg Seebeck coefficient (S)	$2x10^{-4}$	V/K

A. Silaen et al.

To be published in **Proceedings of the ASME 2013 4th Micro/Nanoscale Heat** & Mass Transfer International Conference

December 11-14, 2013, Hong Kong

Collaboration with Prof. Chenn Zhou Purdue Calumet

• TE with today's bulk material can increase power generated in different areas of the boiler by 4.4-7.1%. The overall efficiency of the power plant can increase by ~7%.

Lecture 4.2: Summary

- Cost/efficiency trade off:
 - Importance of heat sink and load resistance cooptimization
- New TE module designs can lower the cost significantly
 - Fractional area coverage of TE elements => heat concentration inside the module)
- High temperature topping cycle thermoelectrics with moderate ZT~0.3-1 can improve power plant efficiency by 2-8%

