

**Fundamentals of Nanotransistors**  
**Unit 3 Homework SOLUTIONS**

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In the Unit 3 lectures, I largely used Maxwell-Boltzmann (nondegenerate) statistics for carriers, because it simplified the calculations but still illustrated the key points. In practice, one would need to include Fermi-Dirac statistics, and that complicates things by bringing in Fermi-Dirac integrals, but the fully degenerate ( $T = 0$  K) case is just as easy to solve as the nondegenerate case, and it is also illustrative of more general principles. In this homework assignment, you will re-do many of the calculations done in the lectures, but this time assuming  $T = 0$  K. Hopefully this will deepen your understanding of the concepts discussed in Unit 3.

- 1) Consider a modern, silicon, N-channel MOSFET with the following parameters:

$$L = 20 \text{ nm}$$

$$C_{inv} = 2.8 \text{ } \mu\text{F}/\text{cm}^2$$

$$\mu_n = 200 \text{ cm}^2/\text{V-s}$$

$$R_s = R_d = 100 \text{ } \Omega - \mu\text{m}$$

$$V_{DD} = 0.7 \text{ V}$$

$$T = 300 \text{ K}$$

$$m^* = 0.19m_0$$

Compute the **ballistic mobility** and compare its value to the scattering limited, bulk mobility,  $\mu_n = 200 \text{ cm}^2/\text{V-s}$ . You may assume non-degenerate (Maxwell-Boltzmann) statistics for electrons. (In the last problem in this HW assignment, we will re-visit this problem assuming fully degenerate carrier statistics.)

**Solution:**

According to Lecture 3.1, the ballistic mobility is given by

$$\mu_B \equiv \frac{v_T L}{2(k_B T/q)}$$

Using the given effective mass and temperature, we find

$$v_T = \sqrt{\frac{2k_B T}{\pi m^*}} = 1.23 \times 10^7 \text{ cm/s}$$

### Unit 3 HW Solutions (continued)

$$\mu_B \equiv \frac{v_T L}{2(k_B T/q)} = \frac{(1.23 \times 10^7) \times 20 \times 10^{-7}}{2 \times 0.026} = 473 \text{ cm}^2/\text{V-s}$$

$$\mu_B = 473 \text{ cm}^2/\text{V-s} > \mu_n$$

We will learn in Unit 4 that when  $\mu_B \gg \mu_n$ , the transistor operates in the diffusive (scattering dominated) limit, and when  $\mu_B \ll \mu_n$ , the transistor operates in the ballistic (no scattering) limit. This transistor, which is typical of modern N-channel Si MOSFETs operates in the quasi-ballistic regime that we will discuss in Unit 4.

- 2) To compute the current in an N-channel MOSFET, we would begin with the Landauer expression,

$$I = (2q/h) \int_{E_1}^{E_2} \mathcal{T}(E) M(E) (f_1 - f_2) dE,$$

Assume that contact one is grounded and that a positive voltage (not necessarily small) has been applied to contact 2. Assume 2D electrons,  $T = 0$  K, that the transmission,  $\mathcal{T}_0$ , is independent of energy, and answer the following questions.

- 2a) Determine the limits of integration,  $E_1$  and  $E_2$ , for the integral in the Landauer expression.
- 2b) Evaluate the integral to obtain an expression for the drain current of an N-channel MOSFET at  $T = 0$  K.

We will see later in this HW assignment that this equation can be used to compute the current of a ballistic MOSFET.

#### **Solution 2a):**

Because of the bias on contact 2 (the drain), the Fermi level is lowered

$$E_{F2} = E_{F1} - qV$$

so

$$E_{F1} > E_{F2}$$

For  $f_1(E)$  at  $T = 0$  K:

$$E < E_{F1} : f_1(E) = 1$$

$$E > E_{F1} : f_1(E) = 0$$

### Unit 3 HW Solutions (continued)

For  $f_2(E)$  at  $T = 0$  K:

$$E < E_{F2} : f_2(E) = 1$$

$$E > E_{F2} : f_2(E) = 0$$

The quantity,  $(f_1 - f_2)$  is non-zero only in the energy range  $E_{F2} < E < E_{F1}$  where  $f_1(E) = 1$  and  $f_2(E) = 0$ . We conclude that the limits of integration should be

$$\boxed{\begin{matrix} E_1 = E_{F2} \\ E_2 = E_{F1} \end{matrix}}$$

$$I = (2q/h) \int_{E_{F2}}^{E_{F1}} \mathcal{T}(E) M(E) (f_1 - f_2) dE$$

#### Solution 2b):

Using the results of 2a), assuming a constant transmission, and that  $f_1(E) = 1$  and  $f_2(E) = 0$  in the energy range of interest, we find:

$$I = (2q/h) \mathcal{T}_0 \int_{E_{F2}}^{E_{F1}} M(E) dE$$

In Lecture 3.2, we learned that

$$M(E) = W M_{2D}(E) = W g_v \frac{\sqrt{2m^* (E - E_C)}}{\pi \hbar} \text{ m}^{-1}$$

(In Lecture 3.2, the bottom the conduction band was taken as  $E = 0$ , i.e., we assumed that  $E_C = 0$  in Lecture 3.2.)

The current becomes

$$I = (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} \mathcal{T}_0 \int_{E_{F2}}^{E_{F1}} (E - E_C)^{1/2} dE$$

$$I = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} \mathcal{T}_0 \left\{ (E_{F1} - E_C)^{3/2} - (E_{F2} - E_C)^{3/2} \right\}$$

Note that there are no channels below  $E_C$  (except for the valence band channels that we are ignoring), so when

$$E_{F1} < E_C$$

$$I = 0$$

### Unit 3 HW Solutions (continued)

and when

$$E_{F1} > E_C \text{ and } E_{F2} = E_{F1} - qV < E_C$$

There are no channels for electrons injected from contact 2, so

$$I = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} T_0 (E_{F1} - E_C)^{3/2}$$

Alternatively, the above equation is valid when  $E_{F1} > E_C$   $qV > E_{F1} - E_C$ .

The complete drain current expression is

$$\begin{aligned} &E_{F1} < E_C \quad qV \geq 0: \\ &I = 0 \\ \\ &E_{F1} > E_C \quad qV < E_{F1} - E_C: \\ &I = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} T_0 \left\{ (E_{F1} - E_C)^{3/2} - (E_{F2} - E_C)^{3/2} \right\} \\ \\ &E_{F1} > E_C \quad qV > E_{F1} - E_C: \\ &I = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} T_0 (E_{F1} - E_C)^{3/2} \end{aligned}$$

- 3) In the Landauer approach, current is proportional to the number of channels in the Fermi window:

$$\langle M \rangle \equiv \int M(E) \left( -\frac{\partial f_0}{\partial E} \right) dE$$

At  $T = 0$  K, this becomes

$$\langle M \rangle = M(E_F)$$

Compute the number of channels for a MOSFET under high gate bias with an electron density of  $n_s = 10^{13} \text{ cm}^{-3}$ . Assume a silicon MOSFET with  $m^* = 0.19m_0$ ,  $g_v = 2$ .

$T = 0$  K, and that  $W = 100$  nm. Assume a small drain bias so that  $E_{F1} \approx E_{F2} = E_F$ .

**Solution:**

$$\text{For parabolic energy bands, we have seen that: } M_{2D}(E) = g_v \frac{\sqrt{2m^*(E - E_C)}}{\pi \hbar}, \text{ so}$$

$$\langle M(E) \rangle = WM_{2D}(E_F) = Wg_v \frac{\sqrt{2m^*(E_F - E_C)}}{\pi\hbar} \quad (*)$$

### Unit 3 HW Solutions (continued)

and we only need to find  $E_F$ . We are given the carrier density, and we can find the Fermi level from the carrier density,

$$n_s = \int_{E_C}^{\infty} D_{2D}(E) f_0(E) dE = \int_{E_C}^{E_F} \left( g_v \frac{m^*}{\pi\hbar^2} \right) (1) dE = g_v \frac{m^*}{\pi\hbar^2} (E_F - E_C)$$

$$(E_F - E_C) = \frac{n_s}{(g_v m^* / \pi\hbar^2)}.$$

Now use this result for the Fermi level in the expression for modes (\*):

$$M(E_F) = Wg_v \frac{\sqrt{2m^* n_s / (g_v m^* / \pi\hbar^2)}}{\pi\hbar} = W \sqrt{2g_v n_s / \pi}$$

Putting in numbers:

$$M(E_F) = W \sqrt{2g_v n_s / \pi} = 100 \times 10^{-7} \sqrt{4 \times 10^{13} / \pi} = 35.7$$

$$\boxed{M(E_F) = 35}$$

This number is rather small, so it is probably better to count modes. There can't be a fraction of a mode, so we truncate 35.7 to 35.

- 4) In Lecture 3.3, we showed that for small drain biases, current is proportional to voltage,  $I = GV$ , and that at  $T = 0$  K:

$$G(T = 0 \text{ K}) = \frac{2q^2}{h} \mathcal{T}(E_F) M(E_F)$$

Show that the solution to problem 2) simplifies to this expected result for small voltages.

#### Solution:

Begin with the solution to problem 2):

$$I = \frac{2}{3} (2q/h) Wg_v \frac{\sqrt{2m^*}}{\pi\hbar} \mathcal{T}_0 \left\{ (E_{F1} - E_C)^{3/2} - (E_{F2} - E_C)^{3/2} \right\}$$

$$I = \frac{2}{3} (2q/h) Wg_v \frac{\sqrt{2m^*}}{\pi\hbar} \mathcal{T}_0 \left\{ (E_{F1} - E_C)^{3/2} - (E_{F1} - qV - E_C)^{3/2} \right\} \quad (*)$$

Now let's expand  $(E_{F1} - qV - E_C)^{3/2}$  for small voltages.

$$f(V) = (E_{F1} - qV - E_C)^{3/2} \approx f(V=0) + \left. \frac{df}{dV} \right|_{V=0} V + \dots$$

Ignoring higher order terms in the Taylor series expansions, we find

### Unit 3 HW Solutions (continued)

$$(E_{F1} - qV - E_C)^{3/2} \approx (E_{F1} - E_C)^{3/2} + \left. \frac{d(E_{F1} - qV - E_C)^{3/2}}{dV} \right|_{V=0} V + \dots$$

$$(E_{F1} - qV - E_C)^{3/2} \approx (E_{F1} - E_C)^{3/2} - \frac{3}{2}(E_{F1} - E_C)^{1/2} qV + \dots$$

$$(E_{F1} - E_C)^{3/2} - (E_{F1} - qV - E_C)^{3/2} \approx (E_{F1} - E_C)^{3/2} - \left\{ (E_{F1} - E_C)^{3/2} - \frac{3}{2}(E_{F1} - E_C)^{1/2} qV \right\}$$

$$(E_{F1} - E_C)^{3/2} - (E_{F1} - qV - E_C)^{3/2} \approx \frac{3}{2} q (E_{F1} - E_C)^{1/2} V \quad (**)$$

Now use (\*\*) in (\*) to find

$$I = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} \mathcal{T}_0 \left\{ \frac{3}{2} q (E_{F1} - E_C)^{1/2} V \right\}$$

$$I = (2q^2/h) \mathcal{T}_0 \left\{ W g_v \frac{\sqrt{2m^* (E_{F1} - E_C)}}{\pi \hbar} \right\} V$$

We recognize the term in curly brackets as  $M(E_{F1})$ , so (\*) can be written as

$$\boxed{I = (2q^2/h) \mathcal{T}_0 M(E_{F1}) V = GV}$$

which is the expected result.

- 5) In Lecture 3.3, we showed that for non-degenerate, Maxwell-Boltzmann, carrier statistics,

$$I_{ON}^{ball} = q n_s v_T \text{ where}$$

$$v_T = \sqrt{\frac{2k_B T}{\pi m^*}}$$

is the nondegenerate uni-directional thermal velocity.

Use the results of problem 2) to determine the ballistic on-current for  $T = 0$  K.

### Unit 3 HW Solutions (continued)

#### Solution:

Begin with the current for large drain bias:

$$E_{F1} > E_C \quad qV > E_{F1} - E_C$$

$$I = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} \mathcal{T}_0 (E_{F1} - E_C)^{3/2}$$

Assume ballistic transport  $\mathcal{T}_0 = 1$ :

$$I_{ON}^{ball} = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} (E_{F1} - E_C)^{3/2} \quad (*)$$

Now we need to relate this to the sheet carrier density,  $n_s$ :

$$n_s = \int_{E_C}^{\infty} \frac{D_{2D}(E)}{2} f_0(E) dE = \int_{E_C}^{E_F} \left( g_v \frac{m^*}{2\pi \hbar^2} \right) (1) dE = g_v \frac{m^*}{2\pi \hbar^2} (E_F - E_C) \quad (**)$$

(As discussed in Lecture 3.3, we divide the density of states by 2 because half the states can be filled by contact 1 and half by contact 2, but under high bias, the Fermi level in so low in contact 2, so that no states are filled by contact 2.)

From (\*) and (\*\*), we find:

$$\begin{aligned} \frac{I_{ON}^{ball}}{qn_s} &= \frac{2}{3} \frac{(2q/h) W g_v}{q} \frac{\sqrt{2m^*}}{\pi \hbar} \frac{(E_{F1} - E_C)^{3/2}}{g_v \frac{m^*}{2\pi \hbar^2} (E_{F1} - E_C)} \quad (***) \\ &= \frac{2}{3} \times \frac{2}{h} W 2\hbar \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} \end{aligned}$$

Now for parabolic energy bands, velocity and energy are related by

$$\frac{1}{2} m^* v(E)^2 = (E - E_C)$$

$$v(E) = \sqrt{\frac{2(E - E_C)}{m^*}}$$

At the Fermi energy, the velocity is

$$v(E_F) = \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} = v_F \quad (****)$$

where  $v_F$  is the so-called Fermi velocity. Using (\*\*\*\*) in (\*\*\*), we find

$$\frac{I_{ON}^{ball}}{qn_s} = W \frac{2}{3} \left( \frac{2}{\pi} v_F \right)$$

### Unit 3 HW Solutions (continued)

We recognize  $\left( \frac{2}{\pi} \right) v_F$  as the average x-directed velocity for electrons at the Fermi level. The factor  $2/3$  comes from averaging the x-directed velocity for all energies from  $E_C < E < E_{F1}$ . We conclude

$$\boxed{\begin{aligned} I_{ON}^{ball} &= W(qn_s) \langle \langle v_x^+ \rangle \rangle \\ \langle \langle v_x^+ \rangle \rangle &= \frac{2}{3} \left( \frac{2}{\pi} v_F \right) \end{aligned}}$$

The first set of brackets,  $\langle \rangle$ , denotes an average over angle at a given energy, which gives the factor,  $2/\pi$ . The second set of brackets,  $\langle \langle \rangle$ , denotes an average over energy and gives the factor,  $2/3$ .

Comparing to Lecture 3.3, we see that the nondegenerate and fully degenerate velocities are

$$v_T = \sqrt{\frac{2k_B T}{\pi m^*}} \rightarrow \frac{2}{3} \left( \frac{2}{\pi} v_F \right) = \frac{2}{3} \left( \frac{2}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} \right)$$

- 6) The ballistic injection velocity is an important quantity for a MOSFET. It is the velocity at the virtual source under high drain bias. Compare the value of the ballistic injection velocity for a typical Si MOSFET computed assuming nondegenerate statistics to the value computed assuming fully degenerate ( $T = 0$  K) statistics. Assume the following parameters:

$$T = 300 \text{ K}$$

$$m^* = 0.19m_0$$

$$g_v = 2$$

$$n_s = 10^{13} \text{ cm}^{-2}$$

#### Solution:

For the nondegenerate case, we use the given effective mass and temperature to find



$$v_{inj}^{ball} = v_T = \sqrt{\frac{2k_B T}{\pi m^*}} = 1.23 \times 10^7 \text{ cm/s}$$

For the fully degenerate case, we make the  $T = 0$  approximation even though we are at  $T = 300 \text{ K}$ . (If the semiconductor is strongly degenerate, this is a reasonable approximation.)

### Unit 3 HW Solutions (continued)

From the result of prob. 5):

$$v_{inj}^{ball} = \frac{2}{3} \left( \frac{2}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} \right) \quad (*)$$

Next, we must determine the location of the Fermi level. Only positive velocity states are occupied under on-current conditions, so only half of the density of states is used:

$$n_s = \int_{E_C}^{\infty} \frac{D_{2D}}{2}(E) f_0(E) dE = \int_{E_C}^{E_F} \left( g_v \frac{m^*}{2\pi\hbar^2} \right) (1) dE = g_v \frac{m^*}{2\pi\hbar^2} (E_{F1} - E_C)$$

Solve for  $(E_{F1} - E_C)$  to find

$$(E_{F1} - E_C) = \frac{2\pi\hbar^2}{g_v m^*} n_s,$$

which can be used in (\*) to find

$$v_{inj}^{ball} = \frac{8}{3\sqrt{\pi}} \frac{\hbar}{m^*} \sqrt{n_s / g_v}.$$

Putting in numbers, we find:

$$v_{inj}^{ball} = \frac{8}{3\sqrt{\pi}} \frac{\hbar}{m^*} \sqrt{n_s / g_v} = 2.05 \times 10^7 \text{ cm/s}$$

$$v_{inj}^{ball}(\text{degenerate}) > v_{inj}^{ball}(\text{nondegenerate})$$

In practice, the injection velocity would be between these two values because at  $n_s = 10^{13} \text{ cm}^{-2}$  the semiconductor is between the non-degenerate and fully degenerate limits. As mentioned in Lecture 3.4, in this case

$$v_{inj}^{ball} = \langle \langle v_x^+ \rangle \rangle = v_T \frac{\mathcal{F}_{1/2}(\eta_{FS})}{\mathcal{F}_0(\eta_{FS})}.$$

When the carrier density is high (which produces a high Fermi energy), then we should also worry about conduction band non-parabolicity and the possibility that upper subbands (with possibly larger effective masses) could be occupied.

- 7) In Lecture 3.4, we derived the following expression for the ballistic channel conductance assuming non-degenerate carrier statistics

$$G_{CH} = W Q_n (V_{GS}, V_{DS}) \frac{v_T}{2(k_B T/q)} (*)$$

Derive the corresponding expression for the fully degenerate ( $T = 0$  K) case. (Remember that ballistic conductance is defined for small drain bias.)

### Unit 3 HW Solutions (continued)

#### Solution:

From the results of problem 4), we have in the ballistic limit

$$I = (2q^2/h) \left\{ W g_v \frac{\sqrt{2m^*(E_{F1} - E_C)}}{\pi \hbar} \right\} V$$

so

$$G = (2q^2/h) \left\{ W g_v \frac{\sqrt{2m^*(E_{F1} - E_C)}}{\pi \hbar} \right\}$$

We also know that

$$n_s = \int_{E_C}^{\infty} D_{2D}(E) f_0(E) dE = \int_{E_C}^{E_F} \left( g_v \frac{m^*}{\pi \hbar^2} \right) (1) dE = g_v \frac{m^*}{\pi \hbar^2} (E_F - E_C)$$

Combining these two results, we find

$$\begin{aligned} \frac{G}{n_s} &= \frac{(2q^2/h)}{g_v \frac{m^*}{\pi \hbar^2} (E_{F1} - E_C)} \left\{ W g_v \frac{\sqrt{2m^*(E_{F1} - E_C)}}{\pi \hbar} \right\} \\ &= W q^2 \frac{1}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} / (E_{F1} - E_C) \end{aligned}$$

which can be re-written as

$$G = W (q n_s) \frac{1}{2(E_{F1} - E_C)/q} \left\{ \frac{2}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} \right\}$$

we recognize the term in curly brackets as the average x-directed velocity as the Fermi energy

$$\langle v(E_F)_x \rangle = \frac{2}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} = \frac{2}{\pi} v_F$$

so the final answer is

$$\begin{aligned}
 G &= W Q_n(V_{GS}, V_{DS}) \frac{1}{2(E_{F1} - E_C)/q} \langle v_x^+(E_{F1}) \rangle \\
 Q_n(V_{GS}, V_{DS}) &= q n_s \\
 \langle v_x^+(E_{F1}) \rangle &= \frac{2}{\pi} v_F
 \end{aligned}$$

### Unit 3 HW Solutions (continued)

Comparing the fully degenerate case to the non-degenerate case, (\*), we see that

$$2(k_B T/q) \rightarrow 2(E_F - E_C)/q$$

$$v_T \rightarrow \langle v_x^+(E_F) \rangle = \frac{2}{\pi} v_F$$

8) The ballistic model we developed in Lecture 3.4,

$$I_{DS} = W |Q_n(V_{GS}, V_{DS})| v_T \left( \frac{1 - e^{-qV_{DS}/k_B T}}{1 + e^{-qV_{DS}/k_B T}} \right)$$

assumed non-degenerate carrier statistics. In this case, the drain current saturates when  $V_{DS} \gg k_B T$ . Answer the following questions about the  $T = 0$  K drain saturation voltage.

8a) Derive an expression for  $V_{DSAT}$ .

8b) Compare nondegenerate and degenerate drain saturation voltages for a silicon MOSFET biased at a gate voltage so that  $n_s = 10^{13} \text{ cm}^{-3}$ .

#### Solution 8a):

From the solution to problem 2b), we found

$$I = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} \mathcal{T}_0 \left\{ (E_{F1} - E_C)^{3/2} - (E_{F2} - E_C)^{3/2} \right\}$$

When

$$E_{F1} > E_C \text{ and } E_{F2} = E_{F1} - qV < E_C$$

there are no channels for electrons injected from contact 2, so

$$I = \frac{2}{3} (2q/h) W g_v \frac{\sqrt{2m^*}}{\pi \hbar} \mathcal{T}_0 (E_{F1} - E_C)^{3/2}.$$

Alternatively, the above equation is valid when  $E_{F1} > E_C$   $qV > E_{F1} - E_C$ .

We conclude that

$$V_{DSAT} = (E_{F1} - E_C) / q \quad (*)$$

The location of the source Fermi level is determined by the mobile charge density in the channel. For  $V_D \geq V_{DSAT}$  only positive velocity states are occupied, so

### Unit 3 HW Solutions (continued)

$$n_s = \int_{E_C}^{\infty} \frac{D_{2D}}{2}(E) f_0(E) dE = \int_{E_C}^{E_{F1}} \left( g_v \frac{m^*}{2\pi\hbar^2} \right) (1) dE = g_v \frac{m^*}{2\pi\hbar^2} (E_{F1} - E_C)$$

from which we find:

$$(E_{F1} - E_C) = \frac{2\pi\hbar^2 n_s}{g_v m^*},$$

which can be used in (\*) to find

$$V_{DSAT} = \frac{(E_{F1} - E_C)}{q} = \frac{2\pi\hbar^2 n_s}{q g_v m^*}$$

### Solution 8b):

Putting in the relevant numbers, we find:

$$V_{DSAT} = 2\pi \frac{\hbar}{q} \frac{\hbar n_s}{g_v m^*} = 0.13 \text{ V}$$

Assume that for the non-degenerate case,  $V_{DSAT} \approx 3 \frac{k_B T}{q} = 0.078 \text{ V}$ .

We conclude that the drain saturation voltage is higher when carrier degeneracy is included.

$$\begin{aligned} V_{DSAT}(\text{nondegenerate}) &= 0.08 \text{ V} \\ V_{DSAT}(\text{degenerate}) &= 0.13 \text{ V} \end{aligned}$$

- 9) Now let's re-visit prob. 1) but this time assuming fully degenerate conditions. Answer the following questions.

- 9a) Derive an expression for the ballistic mobility at  $T = 0$  K. (Remember that mobility is defined for small drain bias.)
- 9b) Numerically evaluate the ballistic mobility for the MOSFET of prob. 1) and compare your answer to the result obtained by assuming nondegenerate conditions.

### Unit 3 HW Solutions (continued)

#### Solution 9a):

In prob. 7), we found the ballistic conductance to be

$$G_B = W(qn_s) \frac{1}{2(E_F - E_C)/q} \left\{ \frac{2}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} \right\}$$

Write this as

$$G_B = n_s q \mu_B \frac{W}{L}$$

and equate the two expressions to find

$$n_s q \mu_B \frac{W}{L} = W(qn_s) \frac{1}{2(E_F - E_C)/q} \left\{ \frac{2}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} \right\}$$

Solve for the ballistic mobility:

$$\mu_B = \frac{L}{2(E_F - E_C)/q} \left\{ \frac{2}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} \right\}$$

which could be written as

$$\mu_B = \frac{\langle v_x^+(E_F) \rangle L}{2(E_F - E_C)/q}$$

#### Solution 9b):

Begin with

$$\mu_B = \frac{L}{2(E_F - E_C)/q} \left\{ \frac{2}{\pi} \sqrt{\frac{2(E_{F1} - E_C)}{m^*}} \right\} (*)$$

Now solve for the location of the Fermi level in terms of the carrier density

$$n_s = g_v \frac{m^*}{\pi \hbar^2} (E_F - E_C)$$

$$(E_F - E_C) = n_s \left( \frac{\pi \hbar^2}{g_v m^*} \right)$$

insert in (\*) to find

$$\mu_B = \frac{2qL}{h} \sqrt{\frac{2g_v}{\pi n_s}}$$

### Unit 3 HW Solutions (continued)

Now insert  $L = 20 \text{ nm}$ ,  $g_v = 2$ , and  $n_s = 10^{13} \text{ cm}^{-2}$  to find

$$\boxed{\mu_B = 345 \text{ cm}^2/\text{V-s}}$$

This should be compared to the value of 473 that was obtained in prob. 1) using nondegenerate carrier statistics. In practice, MOSFETs in the on-state operate between the nondegenerate and fully degenerate limits and the ballistic mobility should be defined in terms of Fermi-Dirac integrals.